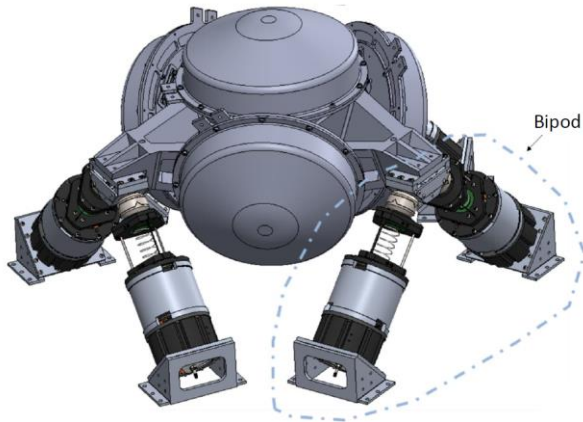
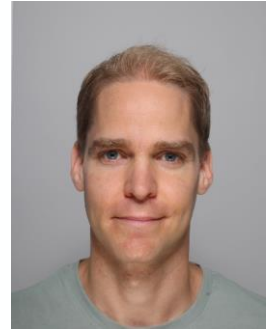


Introduction to *Spacecraft Mechanisms*: ECSS-E-ST-33-01C

Geert Smet
25/10/2023

- Geert Smet
 - Microvibration expert, particularly isolation systems and reaction wheels
 - SADM focal point
 - CleanSpace focal point
 - Almost as fast as Eliud Kipchoge



Terms and Definitions

→ What is a mechanism? Which disciplines are involved?

Scope

→ When is the standard applicable? How to use it?

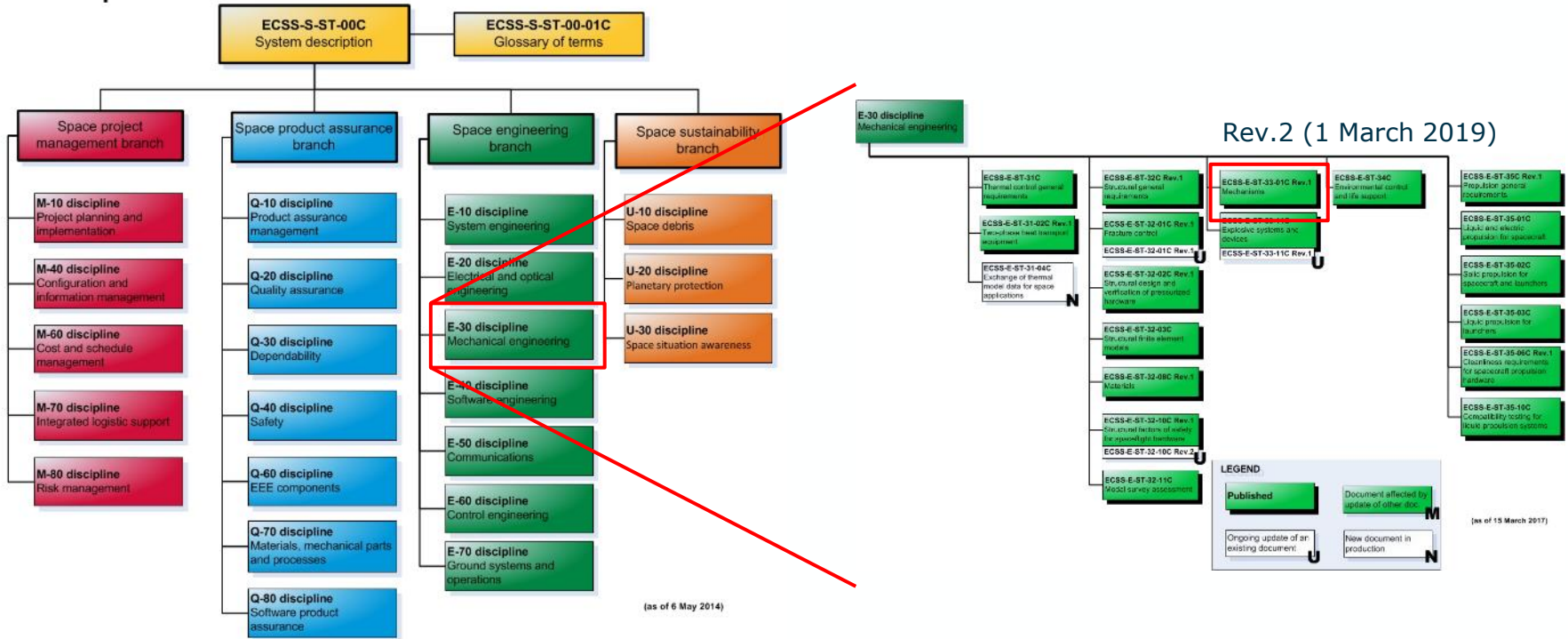
Requirements

→ Design (dimensioning, material selection, etc.)

→ Verification (analysis and test)

Where to find our standards?

ECSS Disciplines



“Assembly of components that are linked together to **intentionally enable a relative motion.**”



Actuators

e.g. electric motor, spring, SMA, voice coil, piezo-electric, etc.

Transmission

e.g. shafts, couplings, gears, etc.

Bearings

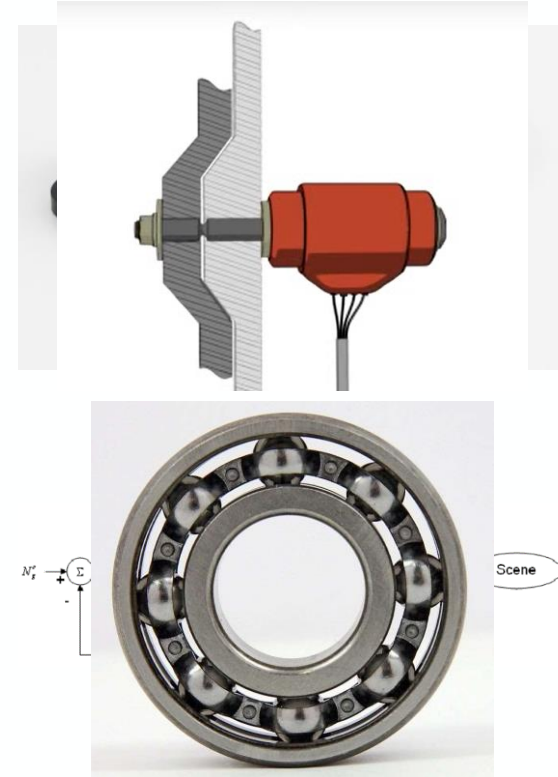
e.g. ball bearings, journal bearings, etc.

Sensors

e.g. optical, magnetic, mechanical, etc.

Controller

open / closed loop, uncontrolled



tribology

discipline that deals with the design, friction, wear and lubrication of interacting surfaces in relative motion to each other

lubrication

use of specific material surface properties or an applied material between two contacting or moving surfaces in order to reduce friction, wear or adhesion

...specifies the **requirements** applicable to the

- concept definition
- development
- design
- production
- verification
- in-orbit operation

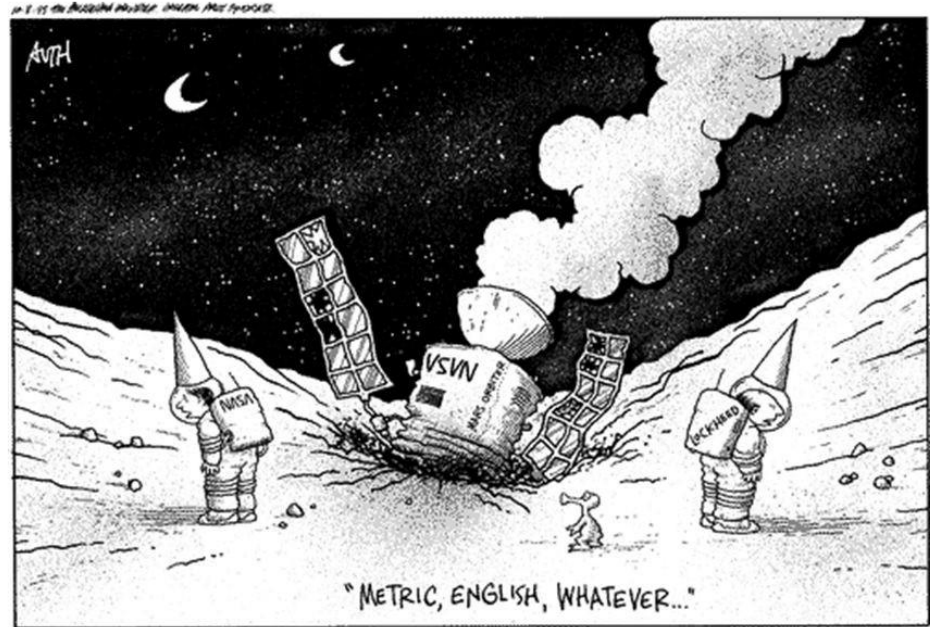
of space mechanisms on spacecraft and payloads
in order to **meet the mission performance requirements.**

Normative references

| | |
|-----------------|--|
| ECSS-S-ST-00-01 | ECSS system — Glossary of terms |
| ECSS-E-ST-10-02 | Space engineering – Verification |
| ECSS-E-ST-20 | Space engineering – Electrical and electronic |
| ECSS-E-ST-20-06 | Space engineering – Spacecraft charging |
| ECSS-E-ST-20-07 | Space engineering – Electromagnetic compatibility |
| ECSS-E-ST-31 | Space engineering – Thermal control general requirements |
| ECSS-E-ST-32 | Space engineering – Structural |
| ECSS-E-ST-32-01 | Space engineering – Fracture control |
| ECSS-E-ST-32-10 | Space engineering – Structural factors of safety for spaceflight hardware |
| ECSS-E-ST-33-11 | Space engineering – Explosive systems and devices |
| ECSS-Q-ST-30 | Space product assurance - Dependability |
| ECSS-Q-ST-40 | Space product assurance – Safety |
| ECSS-Q-ST-70 | Space product assurance – material, mechanical part and process |
| ECSS-Q-ST-70-36 | Space product assurance – Material selection for controlling stress corrosion cracking |
| ECSS-Q-ST-70-37 | Space product assurance – Determination of the susceptibility of metals to stress corrosion cracking |
| ECSS-Q-ST-70-71 | Space product assurance – Data for selection of space materials and processes |
| ISO 76 (2006) | Rolling bearings – Static load rating |
| ISO 128 (1996) | Technical drawings |
| ISO 677 (1976) | Straight bevel gears for general engineering and for |

All units to be used: **SI**

E.g. kinematic viscosity
= [St] Stokes
= $10^{-4} \text{ m}^2 \cdot \text{s}^{-1}$



Remember the Mars Climate Orbiter incident from 1999?

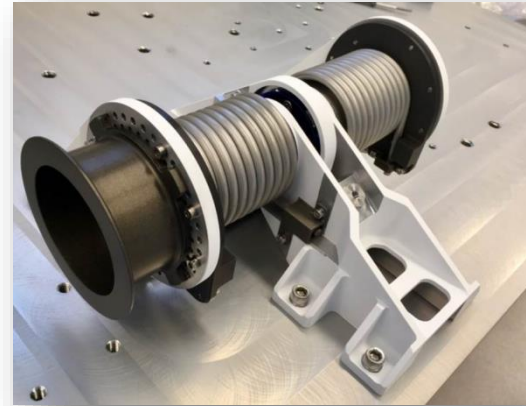
→ Mechanisms shall be designed to be **maintenance free**

→ If maintenance is required, it shall be **approved** by the customer and **procedures** shall be provided

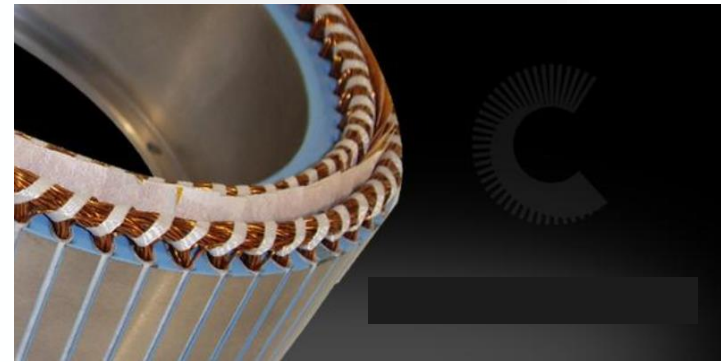


General Requirements: Redundancy

- single point failure modes shall be identified
- single points of failure should be eliminated by **redundant components**
- **active elements** of mechanisms shall be redundant, such as sensors, motor windings, brushes, actuators, switches and electronics



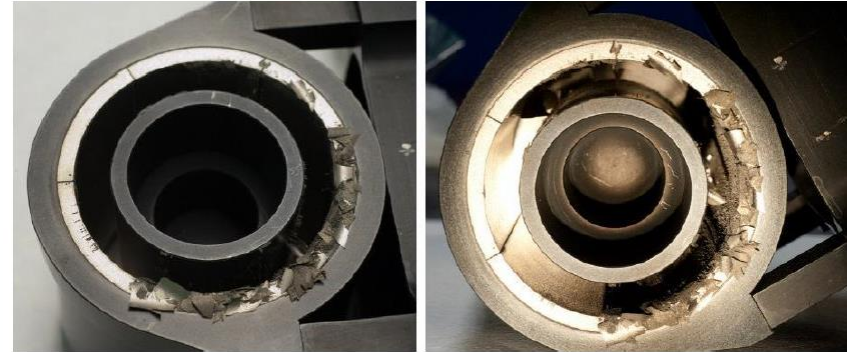
Courtesy of Sener (PL)



<http://www.componeticsinc.com/>

The mechanism engineering shall consider **every mission phase** identified for the specific space programme, i.e.:

- Assembly and integration (humidity, oxygen)
- Testing (1 g environment, additional resistive loads)
- Storage (long term effects)
- Handling and shipment (loads, accessibility)
- Launch (mechanical loads)
- In-orbit operation / hibernation (operational loads, thermal, radiation, EMC, life, etc.)
- End of life / satellite disposal (Design for Demise)

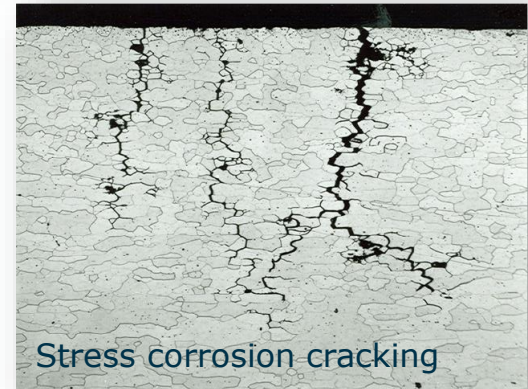


*IASI Voice coil actuator stator,
VACODYM 383 HR (VAC) magnets with Nickel coating*

Material selection

... shall be performed in conformance with **ECSS-Q-ST-70 (Materials)**:

- Corrosion
- **Galvanic corrosion (→ dissimilar metals)**
- **Stress corrosion cracking (e.g. 440C, Cronidur X30)**
- Fungus protection
- Flammable, toxic and unstable materials
- Induced emissions (stray light protection)
- Radiation
- Atomic oxygen
- Fluid compatibility

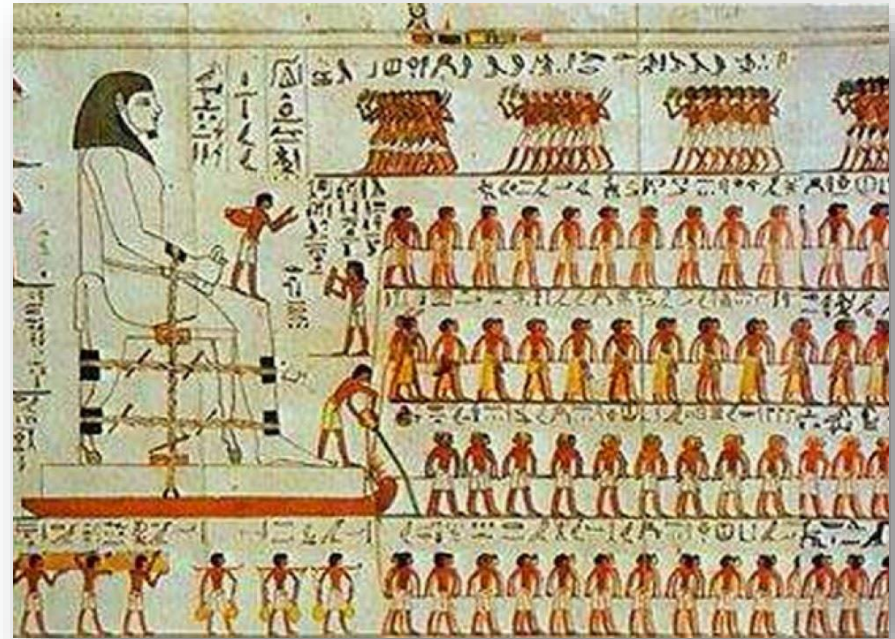


Design Requirements: Tribology

Mechanisms shall:

- be designed with a **lubrication function** between surfaces
 - Reduce friction and wear
 - Increase lifetime
- use only lubricants **qualified for the mission**
 - Temperatures, ambient pressure, contact pressure, number of cycles, lifetime, relative velocity etc.

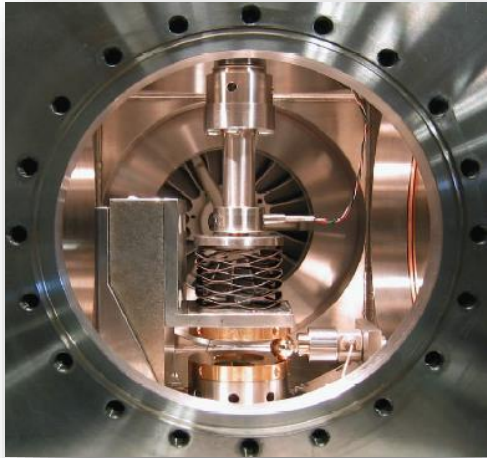
<https://www.esmats.eu/esmatspapers/pastpapers/pdfs/2023/kent.pdf>



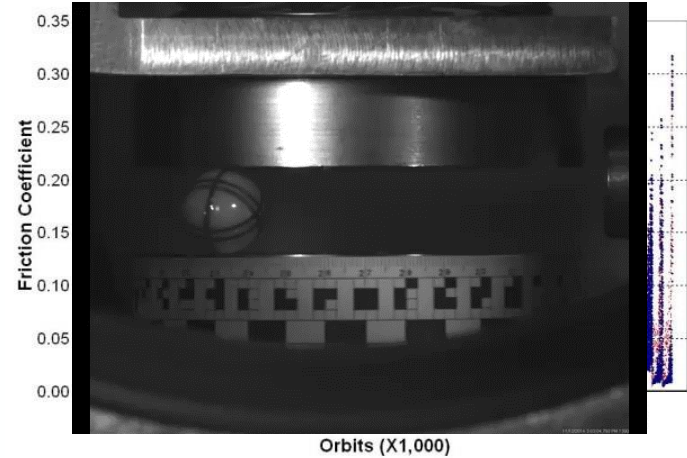
Design Requirements: Tribology (cont'd)

Qualification of lubricant via:

- Heritage or dedicated lifetest (see slides 51 ff.)
- Component level: bearing / gear test rigs, Pin on disc (POD), Spiral orbit tribometer (SOT)



SOT device by ESTL



European Space Tribology Laboratory (ESTL):

- operates test facilities
- has data base on qualified lubricants
- provides consultancy (Minor consultancy is free, paid by ESA)

www.esrtechnology.com

Design Requirements: Dry Lubrication

- ... preferred for operation in **high temperature**, at **low speeds**, **low number of operational cycles**, when **cleanliness** is an issue (e.g. optical payloads have problems with condensation)
 - ... applied through processes such as sputtering, vapor deposition etc.
 - ... e.g. MoS₂, WS₂, graphite, PTFE, lead, gold
-
- Samples of representative material [...] shall be co-deposited in each process with the flight components so that verification checks can be performed;
 - The thickness and adhesion of the lubricant on samples shall be verified;



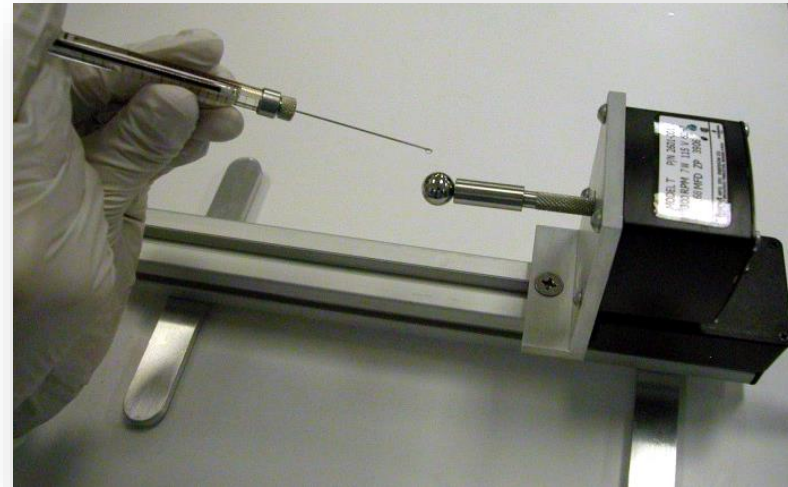
Design Requirements: Fluid Lubrication

... for **high speed**, **low friction** and **high number of operational cycles**

... wide range of space qualified hydrocarbon and synthetic oils

- The **quantity** of lubricant used shall be determined.
- Oil loss mechanisms: **Outgassing**, **creep** and absorption shall be taken into account (including **ground effects**, i.e. gravity)
- Oil budget needs to be established
- For rules on outgassing (total / relative mass loss, collected volatile condensable materials):

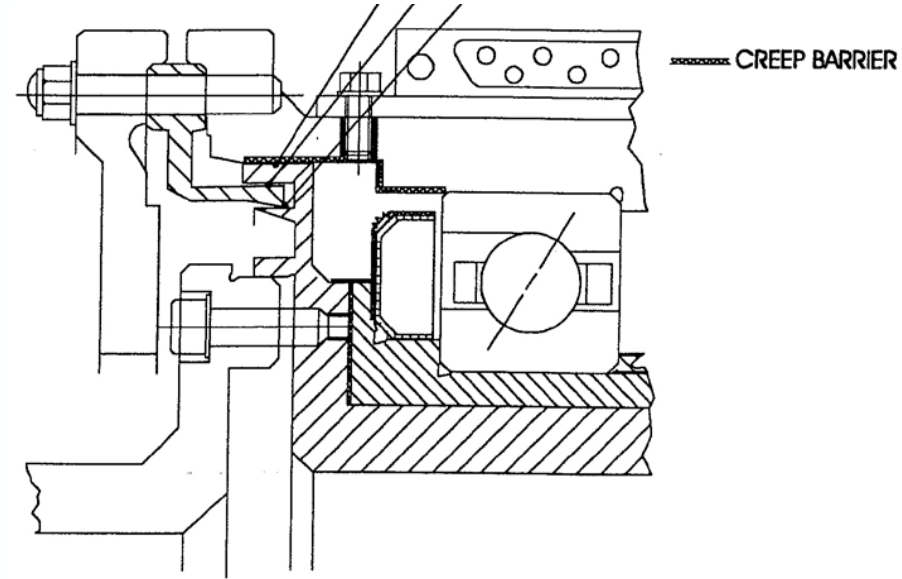
→ **ECSS-Q-ST-70-02**



Courtesy of ESTL

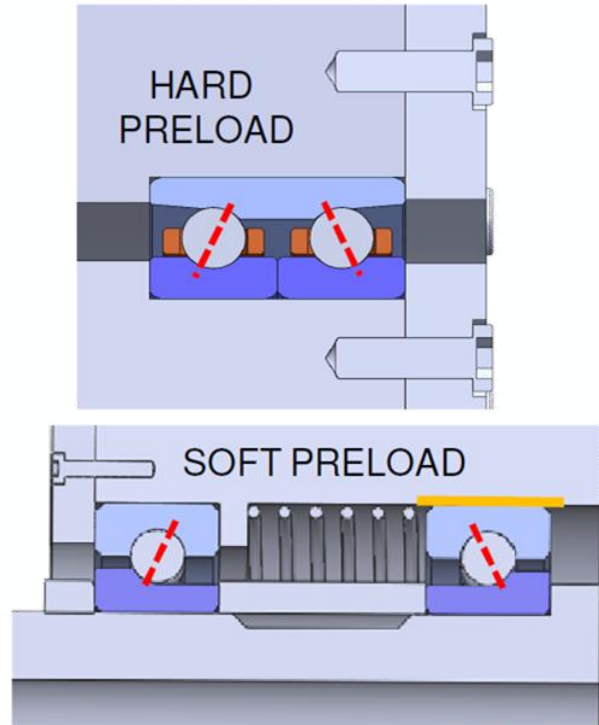
Design Requirements: Anti-creep barriers

- **avoid migration** of fluid lubricants to the internal/external sensitive equipment;
- causes a **change of the lubricant amount** on the parts to be lubricated;
- **integrity** of the anti-creep barrier shall be verifiable by indicators.



Design Requirements: bearing preload

- Ball bearings shall be preloaded to **withstand mechanical environment**;
- Preload **calculation** shall be made available
- Preloading should be applied by **solid or flexible** preload;
- Preload **should be measured** after assembly;
- preload should be confirmed **after running-in**;



Mechanisms shall be designed with a **positive margin of safety** against yielding and against ultimate under all environmental conditions and operational load conditions

→ **ECSS-E-ST-32**

(structures):

4.5.16 Margin of safety (MOS)

a. Margins of safety (MOS) shall be calculated by the following formula:

$$MOS = \frac{\text{design allowable load}}{\text{design limit load} \times FOS} - 1$$

NOTE Loads can be replaced by stresses if the load- stress relationship is linear.

→ **ECSS-E-ST-32-10**

(factors of safety):

$$FOS_Y = 1.1$$
$$FOS_U = 1.25$$

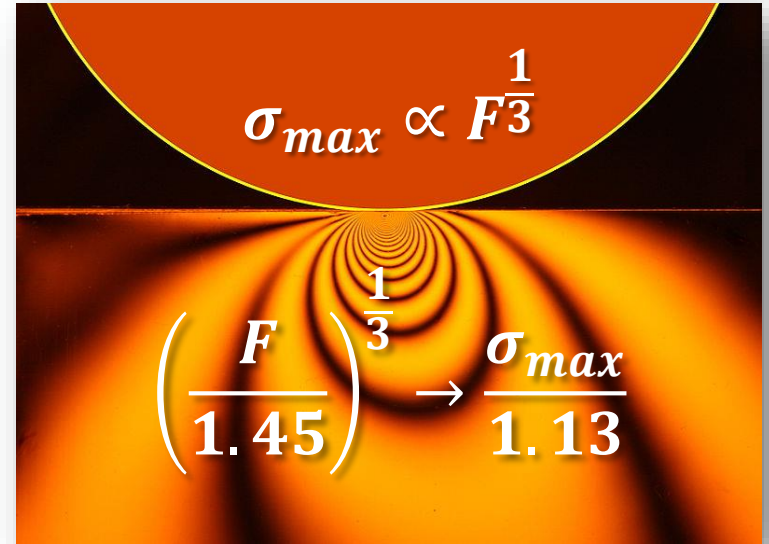
(typical values)

Design Requirements: ball bearings

- shall be sized with respect to the maximum allowable **peak hertzian contact stress**;
- For the evaluation of the peak hertzian contact stress, a minimum **factor of 1.45** shall be applied to the design limit load;

According to **ISO76** (static load rating):

- axial / radial static load capacity \triangleq load producing a maximum contact stress of
4200 MPa (for hardened steels, e.g. SAE 52100)
4000 MPa (for stainless steels, e.g. 440C)



Design Requirements: motorisation

Actuators shall be sized to provide torques / forces in conformance with:

$$T_{min} = 2 \cdot (1.1 \cdot I + 1.2 \cdot S + 1.5 \cdot H_M + 3 \cdot F_R + 3 \cdot H_Y + 3 \cdot H_A + 3 \cdot H_D) + 1.25 \cdot T_D + T_L$$

$$T_{min} \geq 2 \cdot \sum_i (k_i \cdot T_{res,i}) + T_L + 1.25 \cdot T_D$$

- throughout the operational **lifetime** (ageing, lubricant degradation, creep, etc.)
- over the full **range of travel**
- worst case **environmental and operational conditions** (temperatures, mechanical loads)

Design Requirements: motorisation (cont'd)

Actuators shall be sized to provide torques / forces in conformance with:

$$T_{min} = 2 \cdot (1.1 \cdot I + 1.2 \cdot S + 1.5 \cdot H_M + 3 \cdot F_R + 3 \cdot H_Y + 3 \cdot H_A + 3 \cdot H_D) + 1.25 \cdot T_D + T_L$$

$$T_{min} \geq 2 \cdot \sum_i (k_i \cdot T_{res,i}) + T_L + 1.25 \cdot T_D$$

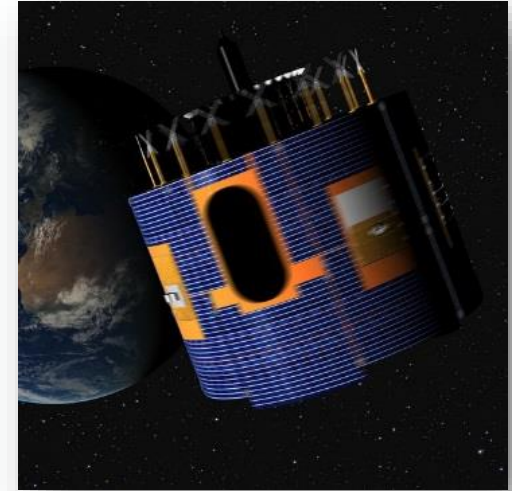
T_L : Deliverable **output torque of the mechanism** when specified by customer

T_D : **inertial resistance torque** caused by the worst-case acceleration function specified by the customer (i.e. customer specifies a motion rather than a torque)

Design Requirements: motorisation (cont'd)

Minimum uncertainty factors for **loss terms**:

| Resistive force or torque contributor | Symbol | Theoretical Factor | Measured Factor |
|---------------------------------------|----------------|--------------------|-----------------|
| Inertia | I | 1,1 | 1,1 |
| Spring | S | 1,2 | 1,1 |
| Magnetic effects | H _M | 1,5 | 1,1 |
| Friction | F _R | 3 | 1,5 |
| Hysteresis | H _Y | 3 | 1,5 |
| Others (e.g. Harness) | H _A | 3 | 1,5 |
| Adhesion | H _D | 3 | 3 |



→ **I** ≠ **T_D**, but resistive inertia load due to acceleration of mechanism itself (e.g. spinning spacecraft!)

→ **S** ≠ **actuation torque**, but resistive spring load (e.g. latch)

Design Requirements: motorisation (cont'd)

If actuation force / torque is supplied by a spring:

- springs shall be redundant (e.g. 1:2 or 2:3 redundancy)
- actuation torque / force shall be multiplied by an uncertainty **factor of 0.8** (→ only if ageing measurements are not available)

If actuation force / torque is supplied by an electric motor:

- Worst case actuation torque / force shall be **measured at operating conditions** (i.e. at representative temperatures, pressures, speeds, loads etc.)
- Assess the failure case with short circuited redundant motor windings

Actuation forces / torques supplied by **devices whose primary function is not to provide actuation** (e.g. harness) shall not be taken into account

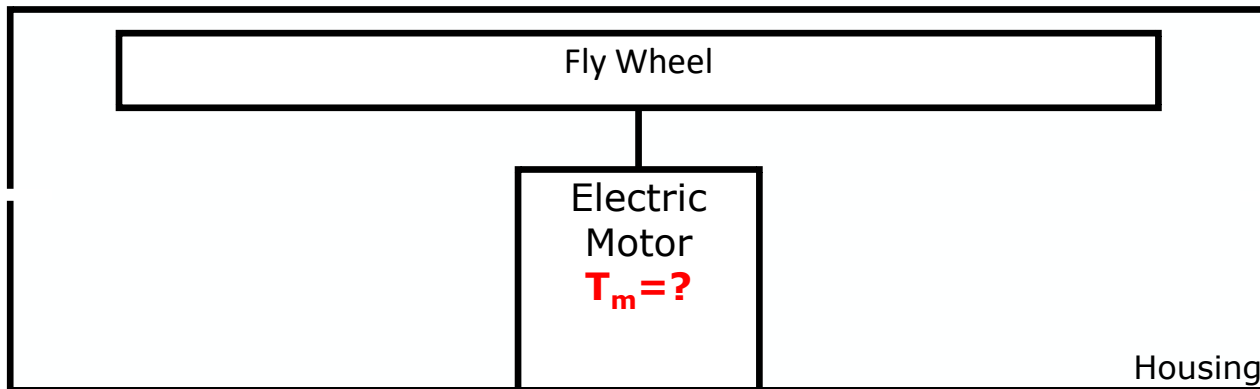
Exercise: Motorisation I

reaction wheel

| | | |
|-----------------------|-----------|--------------------|
| T_{reaction} | = 0.10 Nm | from customer spec |
| T_{friction} | = 0.01 Nm | from data sheet |
| T_{magnetic} | = 0.01 Nm | from analysis |
| T_{Windage} | = 0.02 Nm | from experience |

$$T_{\min} \geq 2 \cdot \sum_i (k_i \cdot T_{\text{res},i}) + T_L + 1.25 \cdot T_D$$

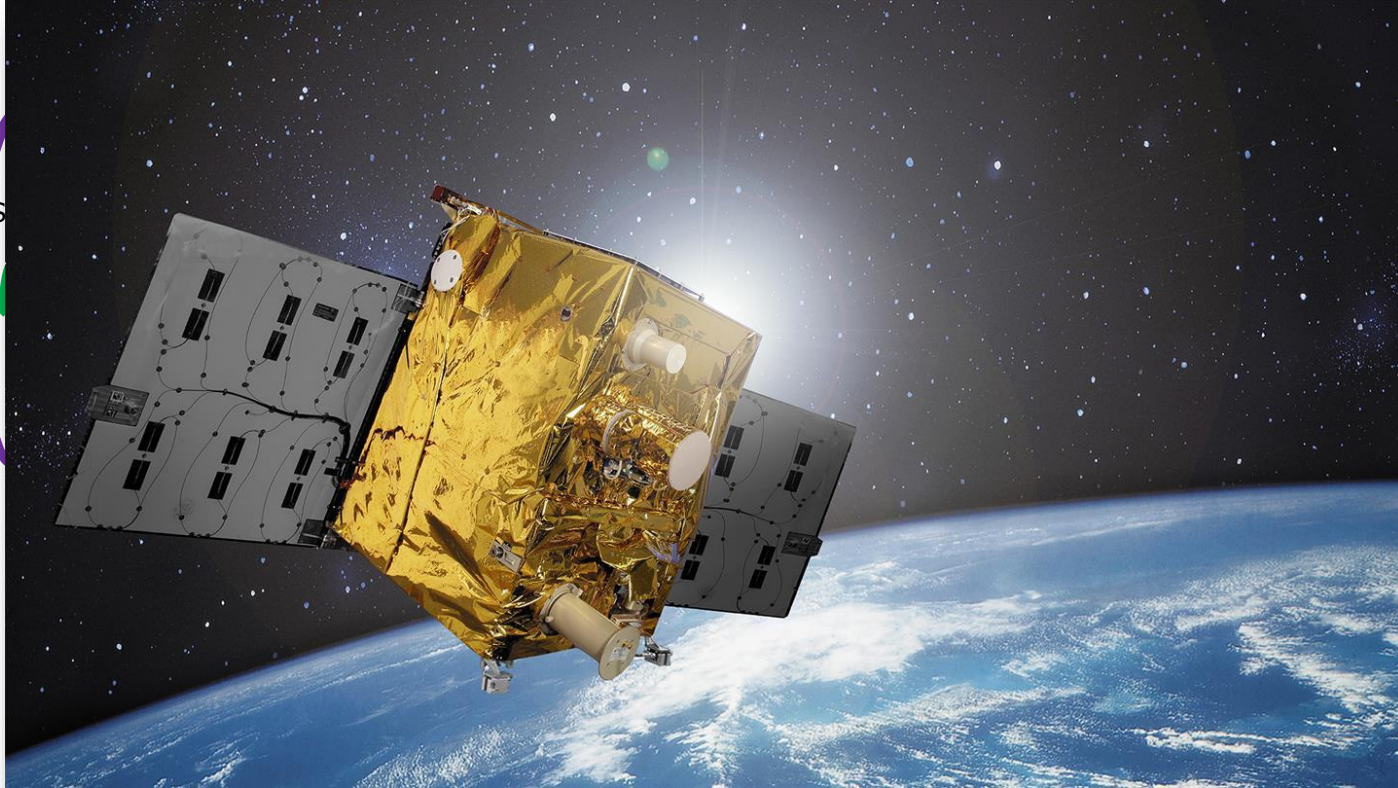
$$T_m = 2 \cdot (1.5 \cdot T_{\text{friction}} + 1.5 \cdot T_{\text{magnetic}} + 3 \cdot T_{\text{windage}}) + T_{\text{reaction}} = 0.295 Nm$$



Exercise: Motorisation II

Spring driven deployment mechanism

Harness



from $Z = 1.5$ m

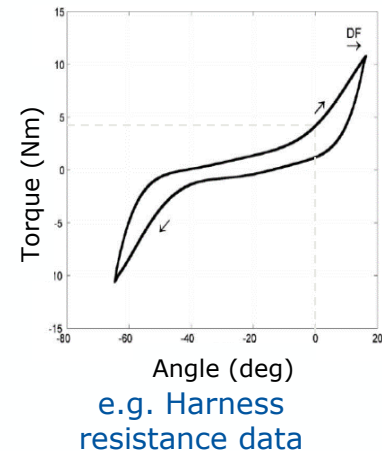
(any axis)
(accelerations)

Exercise: Motorisation II

Spring driven deployment mechanism

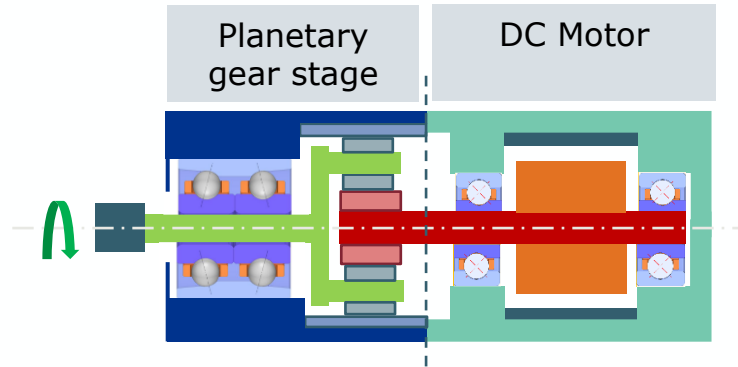
Example Budget:

| Contributor Description | Contributor Origin | Values | Units | ECSS Factor | Factored Contribution | Reference |
|---------------------------------------|----------------------|------------|-----------|-------------|-----------------------|--|
| Inertia | I | 1.5 | Nm | 1.1 | 1.65 | Derived from requirements R2, R3 & R4. |
| Bearing Friction | Friction (FR) | 0.1 | Nm | 1.5 | 0.15 | Tested at bearing level. Report xxx. |
| Damper | Friction (FR) | 0.2 | Nm | 1.5 | 0.3 | Tested at damper level. Report xxx. |
| Latch | Friction (FR) | 0.1 | Nm | 3 | 0.3 | Predicted by analysis. Report xxx. |
| Harness | Other (HA) | 4 | Nm | 1.5 | 6 | Tested on Harness EM. Report xxx. |
| | Magnetic effects | n/a | n/a | n/a | n/a | n/a |
| | Hysteresis | n/a | n/a | n/a | n/a | n/a |
| | Adhesion | n/a | n/a | n/a | n/a | n/a |
| | Dynamic Acceleration | n/a | n/a | n/a | n/a | n/a |
| Total Resistance | | 5.9 | Nm | | 8.4 | |
| Torque including motorisation factor | | | | 2 | 16.8 | |
| Min required torque per spring | Spring | | Nm | 0.8 | 21 | |



Exercise: Motorisation III

DC motor with reduction stage



Example Relevant Requirements:

- R1. Output Torque = 0.2 Nm
- R2. Max commanded speed = 1.5 rads/s
- R3. Max command current = 2 A
- R4. Max command voltage = 24 V
- R5. Temperature range = -20 °C to 30 °C

$$T_{\min} = 2 \times (1,1I + 1,2S + 1,5H_M + 3F_R + 3H_Y + 3H_A + 3H_D) + 1,25T_D + T_L$$

Exercise: Motorisation III

DC motor with reduction stage

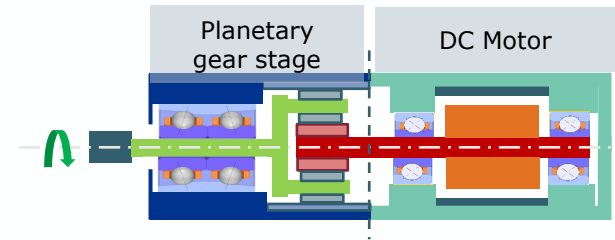
Budget for cold case @ -20 °C

Gear ratio : 8

| Contributor Description | Contributor Origin | Units | Unfactored value at output | ECSS Uncertainty Factors | Factored Contribution @ Output | Factored Contribution @ Motor | Reference |
|--|--------------------------|-----------|----------------------------|--------------------------|--------------------------------|-------------------------------|--------------------------------------|
| Deliverable Output Torque | (T _r) | Nm | 0.20 | 1.0 | 0.20 | 0.025 | Derived from requirement R1 |
| Gearbox output bearings | Friction (FR) | Nm | 0.080 | 1.5 | 0.12 | 0.015 | Tested at bearing level. Report xxx. |
| Planetary gear stage 1 (based on efficiency) | Friction (FR) | Nm | 0.040 | 1.5 | 0.06 | 0.0075 | Tested at gear level. Report xxx. |
| Motor Bearings Uncertainty | Friction (FR) | Nm | - | 1.5-1=0.5 | 0.04 | 0.005 | Tested at bearing level. Report xxx. |
| Total Resistance | | Nm | 0.200 | | 0.22 | 0.028 | |
| Motorisation factor | | | 2 | | 2 | 2 | |
| Total incl. Motorisation factor | | Nm | 0.400 | | 0.44 | 0.055 | |
| Gearbox inertia | Inertial resistance (Td) | Nm | 2.458E-04 | 1.25 | 3.07E-04 | 3.84E-05 | Actuator design report xxx. |
| Min required torque | 0.055 | Nm | | | | | |

This is a “black box” motor case needing caution

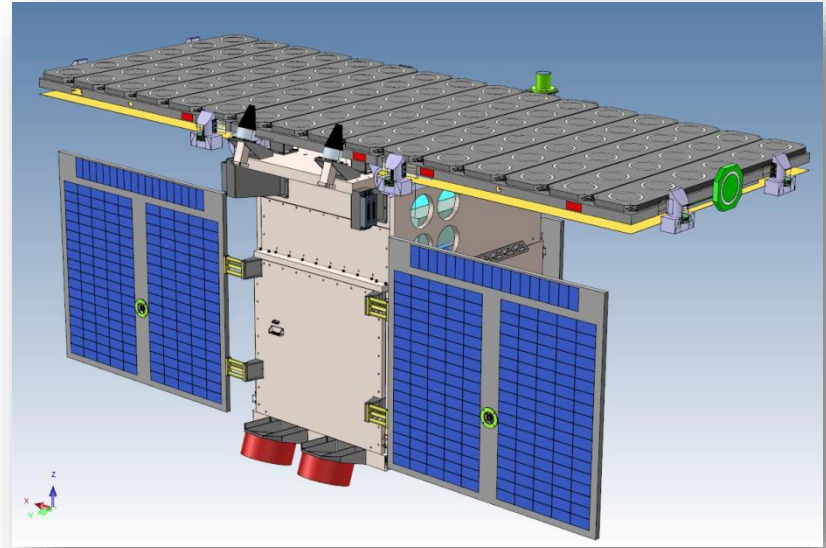
The budget is calculated from output to input to ensure the consequence of output uncertainty is reflected on gears



Design Requirements: end stops

For mechanisms with restricted travel or rotation:

- Use of regular or emergency mechanical end stops (i.e. don't rely on actuator function, e.g. by electric motor)
- deployment indicators shall not be used as mechanical end stops
- Requirements on separable contact surfaces do apply (see next slide)



Courtesy of Qinetiq Space N.V.

Design Requirements: separable contact surfaces

(other than gears, balls and journal bearings)

- maintain adhesion forces below the specified limits
- contact between the mating surfaces shall be characterized
 - surface roughness, hardness, contact geometry
- the peak hertzian contact stress shall be verified to be below 93 % of the yield limit of the weakest material
- avoid potential contact surface property changes
- for metallic surfaces (→ risk of cold welding!):
 - minimum hardness of 500HV
 - use of dissimilar metal (conflict with galvanic corrosion constraints)
 - use of lubricant / dissimilar coatings

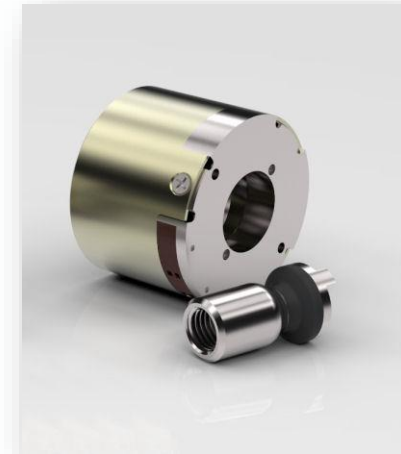
Example: NASA's Galileo High Gain Antenna



- Introduction of a "minor" design change
- Significant increase in hertzian contact pressure (in particular during launch vibrations)
- Lubrication breakdown
- Relative motion in vacuum leading to cold welding between pin and socket
- Partial deployment failure
- Significantly reduced down-link rate

Design Requirements: Threaded parts

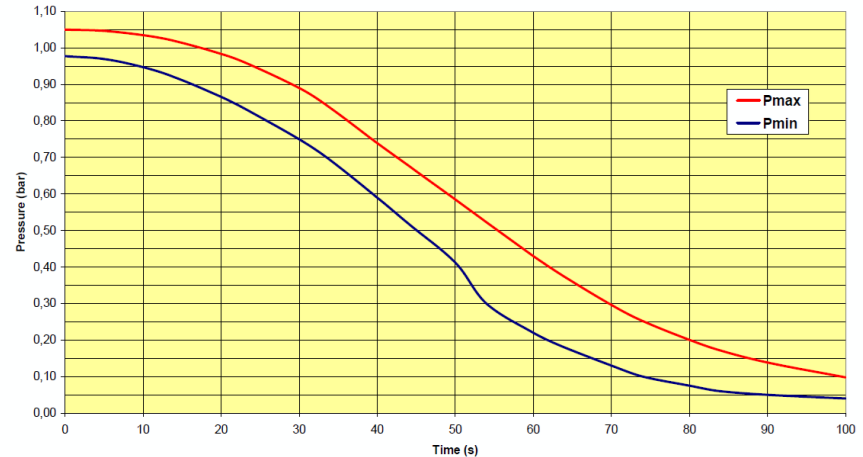
- Use of materials not susceptible to **stress corrosion cracking**
 - Material selection according to ECSS-Q-ST-70-36C
- shall be designed to be **fail-safe** **≠ safe life**
 - **Fracture control** requirements in ECSS-E-ST-32-01C Rev.1
- **preload** shall be justified taking into account **scattering** of all parameters
 - e.g. manufacturing, lubrication and tightening tolerances



<http://www.neaelectronics.com/>

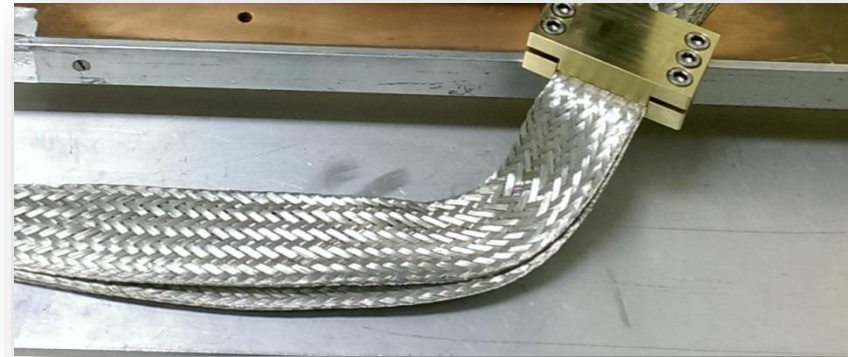
Design Requirements: Venting

- all closed cavities shall be provided with a **venting hole**
- **prevent particles contamination** of bearings, optics and external sensitive components
 - e.g. by means of filters
- **compatibility of the lubricant** with the other spacecraft materials



Design Requirements: Grounding

- Each mechanism shall be **electrically bonded** to the spacecraft structure
- a ground **bonding strap** shall be used between the mechanism housing and the mounting ground plane
- the **length-to-width ratio** of the bonding strap should be smaller than four
- **DC resistance** shall be less than 10 m Ω .



Design Requirements: Others

Other design requirements, regarding:

- Open and closed loop **control systems** (e.g. gain and phase margins)
- Electrical **insulation**
- **Strain** on wires
- Mechanical **clearances** (e.g. MLI support locations)
- Marking and **labelling**
- Flushing and **purging**
- Thermal control (shall be **passive!**)
- **Magnetic cleanliness / EMC**

Verification process in conformance with
ECSS-E-ST-10-02 (Verification)

Review of design, Inspection, Measurement, **Analysis, Test**

→ Verification matrix shall be established

Verification by analysis

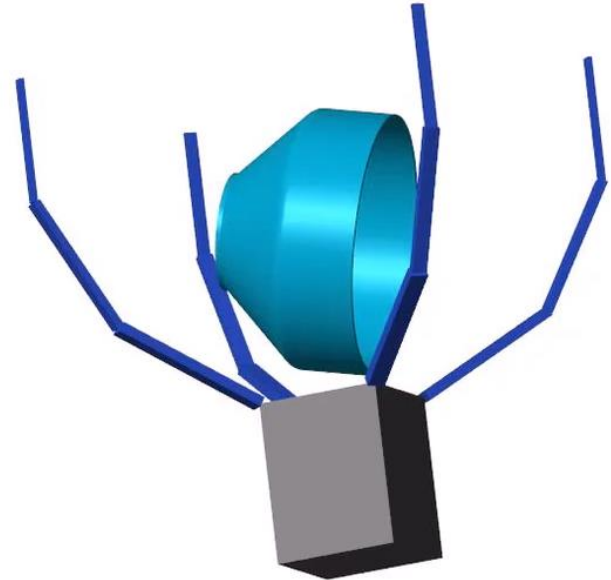
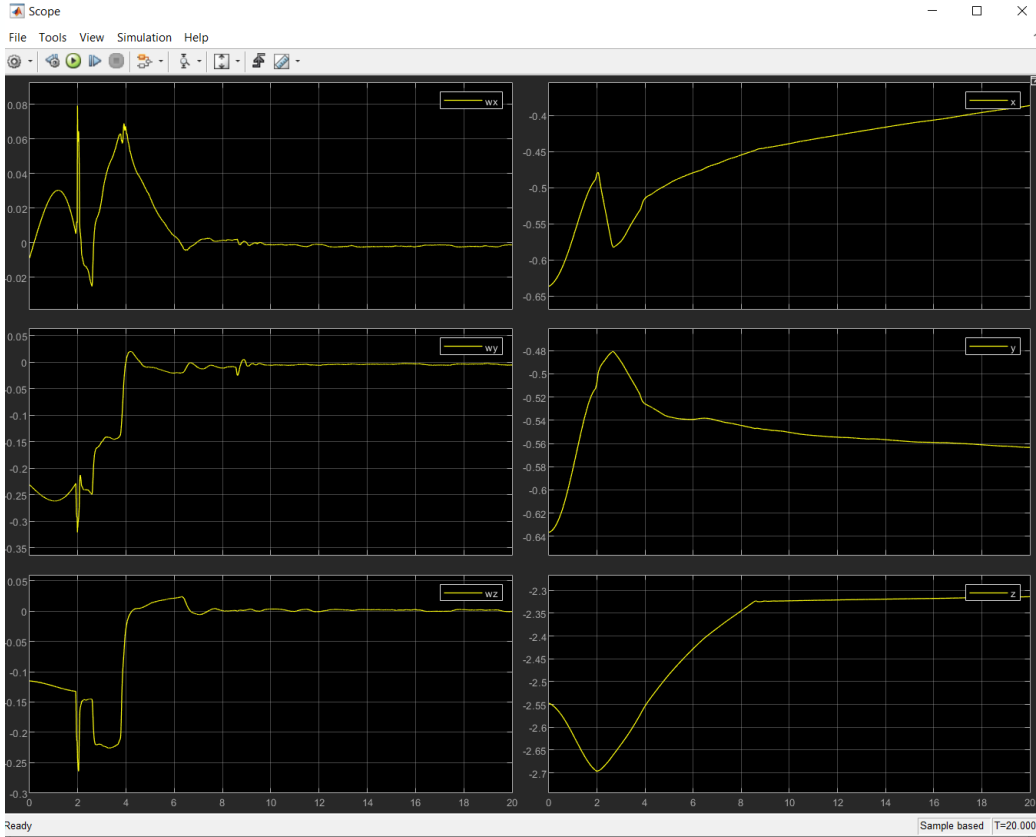
... shall cover extreme conditions

- In flight
- On ground

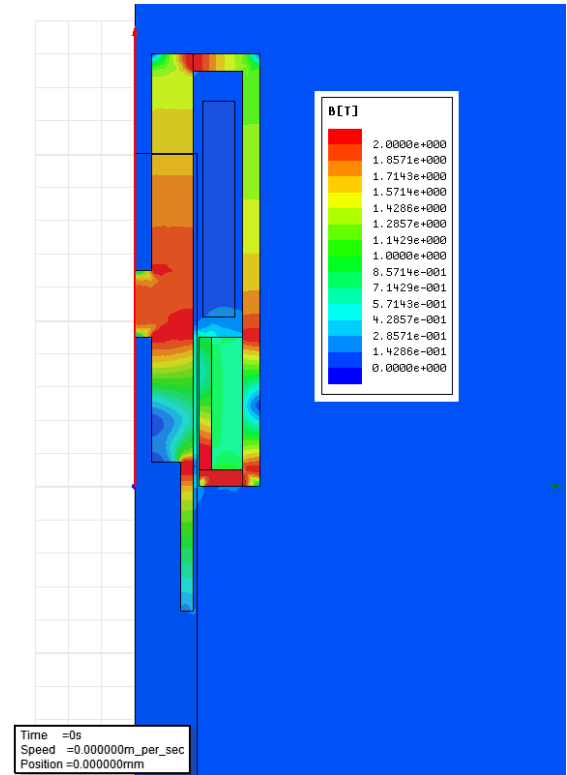
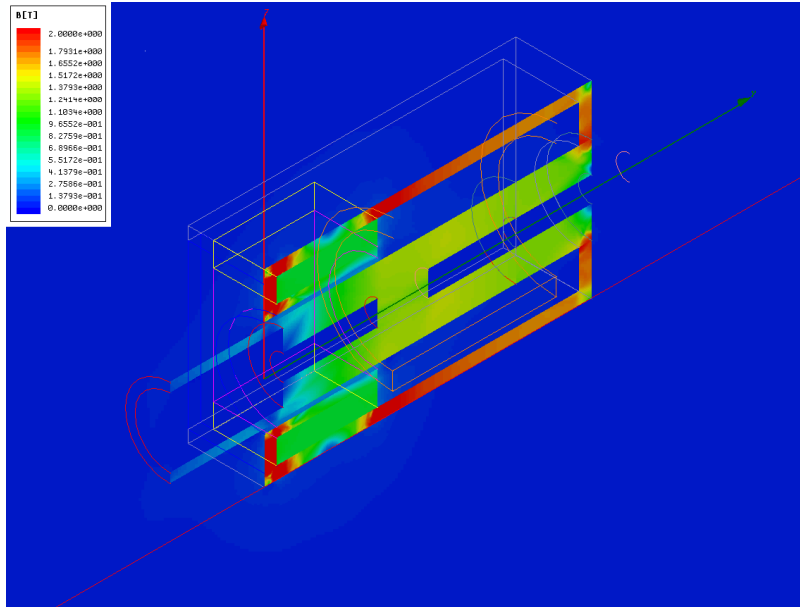
- Thermal analysis
- Structural analysis
- Preload budget
- Functional performance analysis
- Hertzian contact analysis
- Functional dimensioning analysis
- Reliability analysis, FMECA
- Gear analysis
- Shock generation and susceptibility
- Disturbance generation and susceptibility
- Analysis of control systems
- Lubrication analysis
- Lifetime analysis
- Hygroscopic effect analysis
- Magnetic and electromagnetic analysis
- Radiation analysis
- Electrical analysis

- Analytical / numerical model based using, e.g.
 - MS Excel, hand calculation
 - Matlab / Simulink
 - Multi-body simulation tools: Simscape, MSC Adams, Dcap, ...
 - Many more suitable tools
- Verify actuator design / sizing, performance, load generation, motion profile, etc.
- Sensitivity analysis, analyze failure cases
- For deployables / complex robotics systems: main verification technique
- always requires correlation with hardware test data

Functional performance analysis (example)



Example: Polarised Solenoid (Pin Puller)

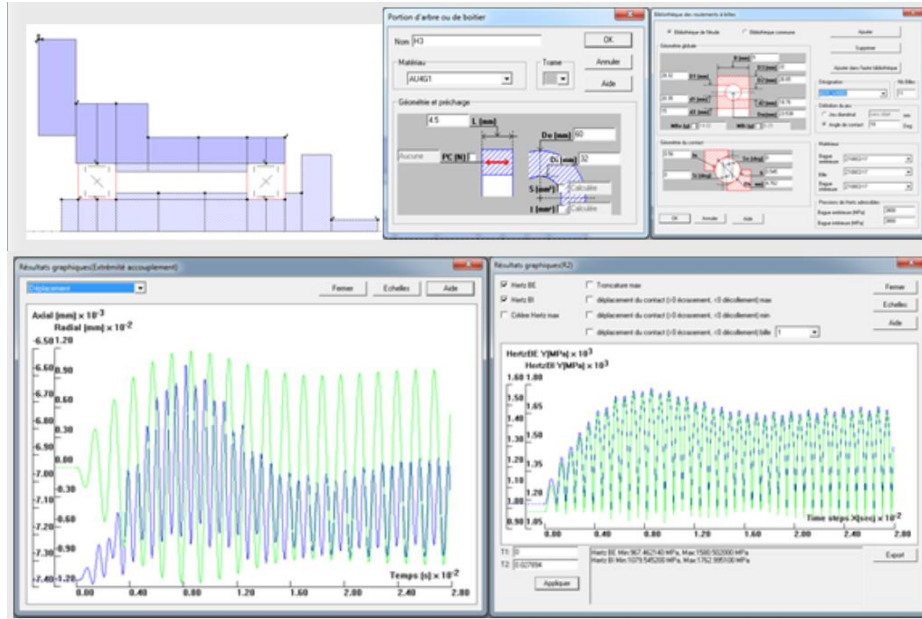


Ball bearing analysis

- Analysis of the **predicted hertzian contact stress** to verify the compliance with the material allowable
- Analysis to verify **sizing of ball bearings** in conformance with the allowable peak hertzian contact stress

- Ball bearing analysis tools: CABARET, RBSDyn, KISSsoft, ORBIN
- Also for separable contact surfaces, gears, end stops

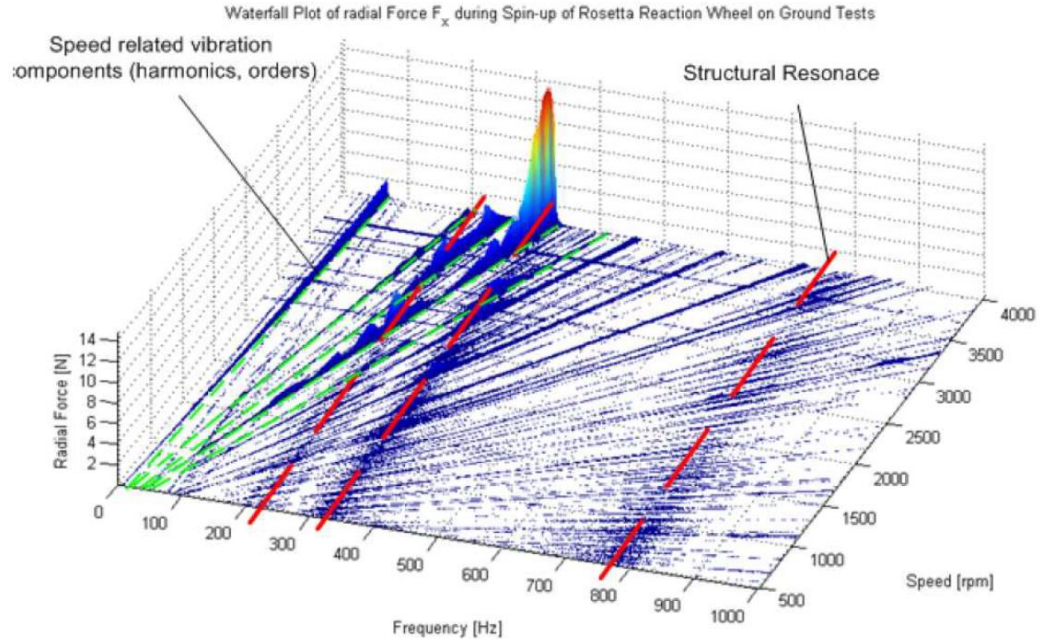
RBSDYN by CNES



source: <https://logiciels.cnes.fr/en/node/56?type=desc>

Example: Microvibration generation of reaction wheels

- Bearing geometry
- Unbalance
- Structural resonances (e.g. FEM model)
- Control frequencies
- Rotor dynamics



$$FTF = \frac{f_r}{2} \cdot \left(1 - \frac{d}{D} \cdot \cos \alpha \right)$$

e.g. Fundamental train frequency

Analysis of quantity of liquid lubrication based on

- partial / ambient pressure
- temperature
- design of labyrinth seal

Potential Oil Loss Mechanisms:

Creep, centrifugal forces, evaporation, absorption by porous materials

$$\frac{dm}{dt} = (p_v - p_p) \sqrt{\frac{M}{2 \cdot \pi \cdot R \cdot T}}$$

e.g. Langmuir equation to analyse oil loss by evaporation

$$\frac{dm}{dt} = \frac{(p_i - p_o) \cdot d \cdot b \cdot v}{(4 + \frac{1.5}{b})}$$

e.g. mass flow over labyrinth seal according to Space Tribology Handbook (ESTL)

Verification by test

- The tests to be performed shall be
 - Defined in a test plan
 - Agreed by the customer
- conformance to ECSS and mechanisms specification
- conformance to functional dimensioning
- performance in launch and operation configuration
- thermal verification
- structural verification
- characterize the dynamic behavior

- Characterisation testing
- Qualification testing
- Acceptance testing

Characterisation testing

- Breadboard model testing during Phase A or B
- Gain confidence in technology (no flight representative hardware)
 - Functional performance test
 - Vibration and thermal tests
 - Tribological lifetime test on critical items
(Example: usage of certain lubricant in bearing / gear test rig)

→ **No formal qualification!**

Table 5-1: Space segment equipment - Qualification test baseline

| Test | Reference clause | Ref. to Level & Duration | Applicability versus types of space segment equipment | | | | | | | | | | | Application notes | | | |
|---------------------------------------|------------------|--------------------------|---|---|---|---|---|---|---|---|---|---|---|-------------------|---|---|---|
| | | | a | b | c | d | e | f | g | h | i | j | k | | | l | |
| General | | | | | | | | | | | | | | | | | |
| Functional and performance (FFT/RFT) | 5.5.1.1 | | R | R | R | R | R | R | R | R | R | R | R | R | R | R | For k (solar array), the deployment test is mandatory before and after the environmental tests (manual deployment before the environmental tests). |
| Humidity | 5.5.1.2 | | X | X | X | X | X | X | X | X | X | X | X | - | X | | For k (solar array) and l (solar panel), see ECSS-E-ST-20-08. |
| Life | 5.5.1.3 | See Table 5-2 No 1 | X | X | R | R | X | X | R | X | X | R | - | - | | | To be performed on dedicated model. For l (solar panels), the life tests are covered by the ECSS-E-ST-20-08. |
| Burn-in | 5.5.1.4 | | X | - | - | X | - | - | X | - | - | - | - | - | | | The test is performed in parallel with other funct. & environm. tests. |
| Mechanical | | | | | | | | | | | | | | | | | |
| Physical properties | 5.5.2.1 | | R | R | R | R | R | R | R | R | R | R | R | R | R | | Upon agreement with customer the CoG and Mol is not measured by test but calculated. |
| Static load | 5.5.2.2 | See Table 5-2 No 2 | X | X | X | X | X | X | X | X | X | X | X | - | | | One of the three types of test is performed if not covered by the sinusoidal vibration test. |
| Spin | 5.5.2.2 | See Table 5-2 No 3 | X | X | X | X | X | X | X | X | X | X | X | - | | | |
| Transient | 5.5.2.2 | See Table 5-2 No 4 | X | X | X | X | X | X | X | X | X | X | X | - | | | |
| Random vibration | 5.5.2.3 | See Table 5-2 No 5 | R | X | R | R | R | R | R | R | X | X | X | - | | | For k (solar array), the random vibration test should be added to acoustic test for fixed solar array mounted directly to the spacecraft side wall (without offset bracket). |
| Acoustic | 5.5.2.4 | See Table 5-2 No 6 | - | X | - | - | - | - | - | - | X | X | R | - | | | For b (antennas), i (optical), j (mechanism), random vibration or, acoustic or both tests are selected depending on the type, size and location of the space segment equipment. |
| Sinusoidal vibration | 5.5.2.5 | See Table 5-2 No 7 | R | R | R | R | R | R | R | R | R | R | R | - | | | |
| Shock | 5.5.2.6 | See Table 5-2 No 8 | R | X | R | R | R | X | R | X | R | R | - | - | | | If it is demonstrated that the susceptibility to shock of the space segment equipment is above the shock environment, the test needs not to be performed. For k (solar array) shock qualification is performed at components level and confirmed during the deployment test. |
| Micro-vibration generated environment | 5.5.2.7 | | X | X | - | X | X | - | X | - | - | X | - | - | | | Test to be performed only if need is identified by analysis. |
| Micro-vibration susceptibility | 5.5.2.8 | See Table 5-2 No 9 | X | - | - | - | - | - | - | - | X | X | - | - | | | Test to be performed only if need is identified by analysis. |
| Structural integrity | | | | | | | | | | | | | | | | | |
| Leak | 5.5.3.1 | See Table 5-2 No 10 | X | - | R | R | R | R | X | X | - | - | - | - | | | Leak and pressure tests may be combined. |

Flight representativeness regards:

- ⚙️ *Design (dimensions, tolerances, surface properties)*
- ⚙️ *Part quality*
- ⚙️ *Materials*
- ⚙️ *Processes*
- ⚙️ *Pre-conditioning (accept. test, run-in)*
- ⚙️ *Operation (e.g. speed profile, control, duration)*

→ The life test model shall be equal to the FM, **but shall not be the FM**

→ Best practice: **life qualification on the QM**



- ⚙ **Wear out**
- ⚙ **Accumulation of wear**
- ⚙ **Pitting**
- ⚙ **Fretting**
- ⚙ **Material fatigue**
- ⚙ **Settling**
- ⚙ **Defect propagation**
- ⚙ **Lubricant deterioration**
(e.g. oil separation, chemical reaction)
- ⚙ **Oil loss**
(e.g. migration, evaporation, absorption, diffusion)
- ⚙ **Creep**

- ⚙ **radiation effects**
- ⚙ **thermal effects**
- ⚙ **electromigration**
- ⚙ **storage effects**

*not addressed by
ECSS-E-ST-33-01C*



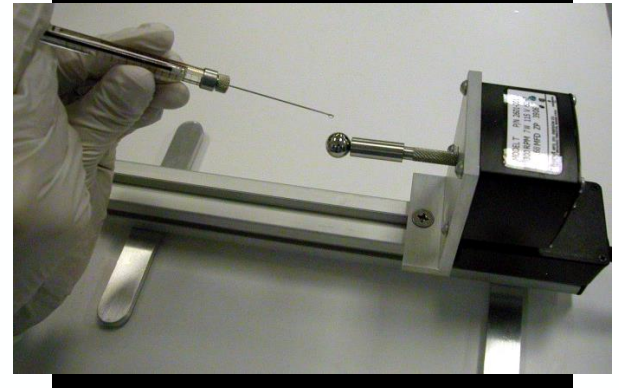
1. Flight-representative assembly and integration

e.g. pre-loading, lubricant quantity and application process etc.

2. Run-in and thermal settling (cycling)

3. Vibration testing

(ECSS-E-ST-33-01C, para. 4.8.3.3.11 b)



$1 \times \text{qual. test} + n \times (\text{accept.}) \text{ test}$

Including sub-system and system level tests!

“ [...] shall be verified using the factored sum of the predicted nominal ground test cycles [...] and the in-orbit

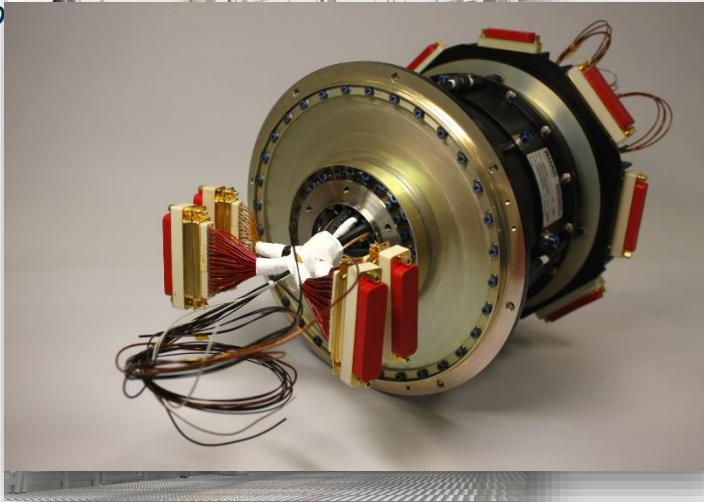


Table 4-4: Life test duration factors

| | Number of expected cycles | Factor |
|------|---------------------------|--------|
| s to | 1 to 1000 cycles | 4 |
| | 1001 to 100 000 cycles | 2 |
| | > 100 000 cycles | 1,25 |
| | 1 to 10 cycles | 10 |
| | 11 to 1000 cycles | 4 |
| | 1001 to 100 000 cycles | 2 |
| | > 100 000 cycles | 1,25 |

| | e.g. SA deployment | e.g. SADM |
|------------------------|-------------------------|---|
| No. of in-orbit cycles | 1 | 29219 |
| on-ground | 2 | 320 |
| lifetest | $1 \times 10 + 10 = 20$ | $10 \cdot 10 + 990 \cdot 4 + 28219 \cdot 2 + 10 \cdot 10 + 320 \cdot 4 = 61878$ |

- Acceleration: Increasing the rate of ageing by increasing of stress factors by a known amount!

➤ Example: compressed test (with long periods of pointing, so)

Stress factors

temperature

contact stress

current density

temperature cycles

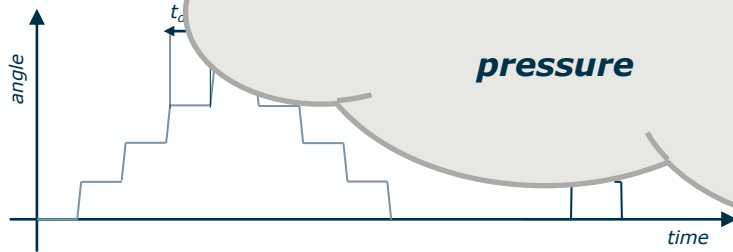
radiation

speed

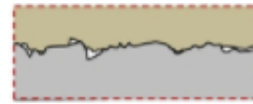
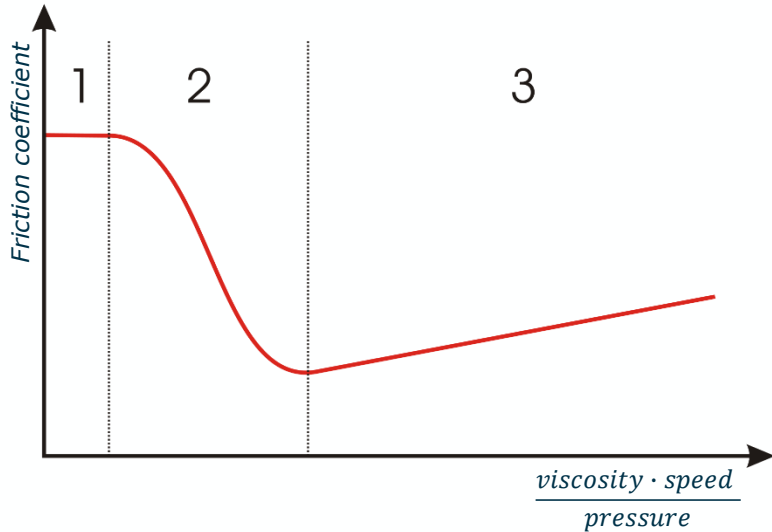
voltage

pressure

operational frequency



operational level
effects & modes are the same
nominal operational level



boundary lubrication
*continuous asperity contact
high friction and wear rate*



mixed lubrication
*some asperity contact
fluid film carries load*



hydrodynamic lubrication
*no metal-to-metal contact
viscous friction*

From [9] for elliptical contacts:

$$U = \eta_0 * \frac{v}{E' R_x}$$

$$G = E\alpha$$

$$W = \frac{F}{E' R_x^2}$$

$$k = \frac{a}{b} \text{ (ellipticity parameter)}$$

η_0 = Base viscosity of lubricant

E' = reduced elastic modulus

F = elliptic integral (= $1.5277 + 0.60.23 \ln(R_x/R_y)$)

α = Lubricant pressure – viscosity coefficient

a, b = Hertzian contact semi – minor and semi – major dimensions

The λ -ra

With

$\lambda > 10$:

$10 > \lambda \geq 3$:

$0.8 < \lambda < 3$:

$\lambda \leq 0.8$:



➤ General

- ⚙️ *Life test as much as possible flight representative*
- ⚙️ *Every deviation from flight condition to be carefully assessed*

➤ Accelerated testing

- ⚙️ *Numerous ageing effects and failure modes*
- ⚙️ *Stress factors contribute differently*
- ⚙️ *Ageing effects shall remain representative*
- ⚙️ *Acceleration by increased*
 - *Frequency of operation: OK (unless very long standstill)*
 - *Temperature: NOK*
 - *Speed: OK for fluid and dry lube; NOK for greases*
 - *Other stress factors: check case-by-case*

Disassembly and visual inspection of tribological parts:

- No direct contact between metallic parts
- Surface properties of contact surfaces not modified beyond specified limits
- No chemical deterioration beyond the specified limits of fluid lubricants
- Amount and size of wear acceptable (performance, contamination)
- Resistive torques according to 4.7.5.3. (motorization)
- Less than 50% degradation of resistive torques / forces
- Performance according to spec

Acceptance testing

- Tests to confirm that flight hardware free from manufacturing defects;
- Test content according to ECSS-E-ST-10-03C, table 5-3;
- Vibration levels and thermal loads which are higher than expected in flight but less than qualification
- Refurbishment should not be performed after successful acceptance testing



Thank you for your attention!

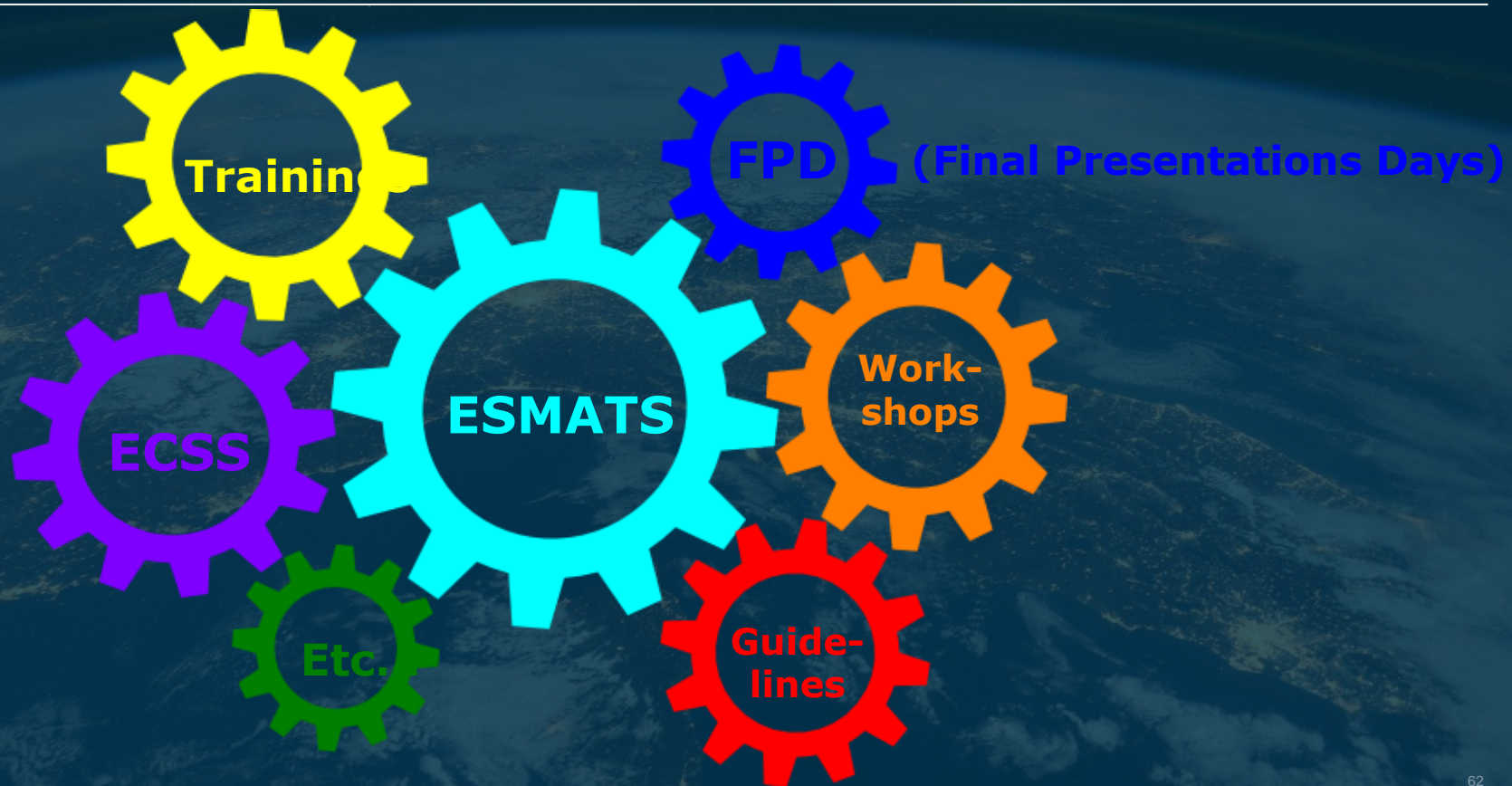
Contact: geert.smet@esa.int





ESA Mechanisms team today
 22 FTE (15 Staffs / 7 Contractors) + 1 integrated support
 1 YGT, 1 trainee
 10 different nationalities...





- 2009 – WS#1 - Hold-Down and Release Mechanisms
- 2010 – WS#2 - Multi-Body simulation
- 2011 – WS#3 - Pyrotechnics
- 2012 – WS#4 - Tribology
- 2013 – WS#5 - Electromagnetic devices
- 2014 – WS#6 - Micro-vibrations
- 2015 – WS#7 - Ball-bearings
- 2016 – WS#8 - Gear technology
- 2017 – WS#9 - Workshop on Mechanisms Testing and Health Monitoring
- 2018 – WS#10 - Optical Mechanisms
- 2019 – WS#11 - Space Mechanisms Legacy from New ESA players
- 2020 – WS#12 - Pyrotechnics and Ball Bearing software (2 workshops in parallel)
- 2021 – WS#13 - Position Sensors
- 2022 – WS#14 - Mechanisms Microvibrations
- 2023 – WS#15 - Mechanisms for CubeSats and MicroSats
- 2024 – WS#16 – CleanSpace 11PM&12AM/03/2024



(Participation limited to ESA member states and cooperating states)

A final presentation is mandatory/requested at the end of any ESA R&D contracts

Instead of organising a final presentation at the end of each R&D contract, we proposed since more than 25 years to

- Merge all final presentations in to a single event, to share **more detailed** information in front of a **bigger audience** / **Space mechanisms community**
- Promote your latest R&D to potential customer
- Promote Networking
- Stimulate Ideas / Partnership for future R&D

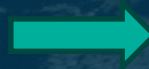


Next event planned 12PM&13/03/2024

(Participation limited to ESA member states and cooperating states)



- AOCS Sensors and Actuators (Reaction Wheels & CMG's)
- Actuators Building Blocks for Mechanisms (Covering now Electric motors, actuators, gears (as before) and position sensors)
- Electric Propulsion Pointing Mechanisms (EPPM)
- Hold Down, Release, Separation and Deployment System
- Pyrotechnics Devices
- Solar Array Drive Mechanisms (SADM)
- Deployable Booms (*now on hold*)



Toward harmonised Roadmaps between you and us

(Participation limited to ESA member states and cooperating states)

Already released:

- Electric Motors For Space Applications Handbook
- Ball-bearing design assembly and preloading operations
- Accelerated testing of liquid Lubricated Mechanisms
- Sizing of an actuator with a gearbox in the drive unit
- Consideration for Long Term Storage of Mechanisms
- Space mechanisms Micro-Vibration Handbook
- Gear handbook Part 1 (Harmonic Drives)
- Pyrotechnics handbook Part 1 (Pyrotechnics devices)



More to come: (feel free to propose new ones)

- Gears handbook Part 2 (Spur gears)
- Pyrotechnics Part 2 (Lessons learned)
- CuBeSat mechanisms Guideline

(Participation limited to ESA member states and cooperating states)



20th European Space Mechanisms and Tribology Symposium Warsaw, Poland



ESMATS 2023

OVERVIEW ▾

AGENDA

TRAINING COURSES ▾

ASTRONIKA

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EXHIBITORS

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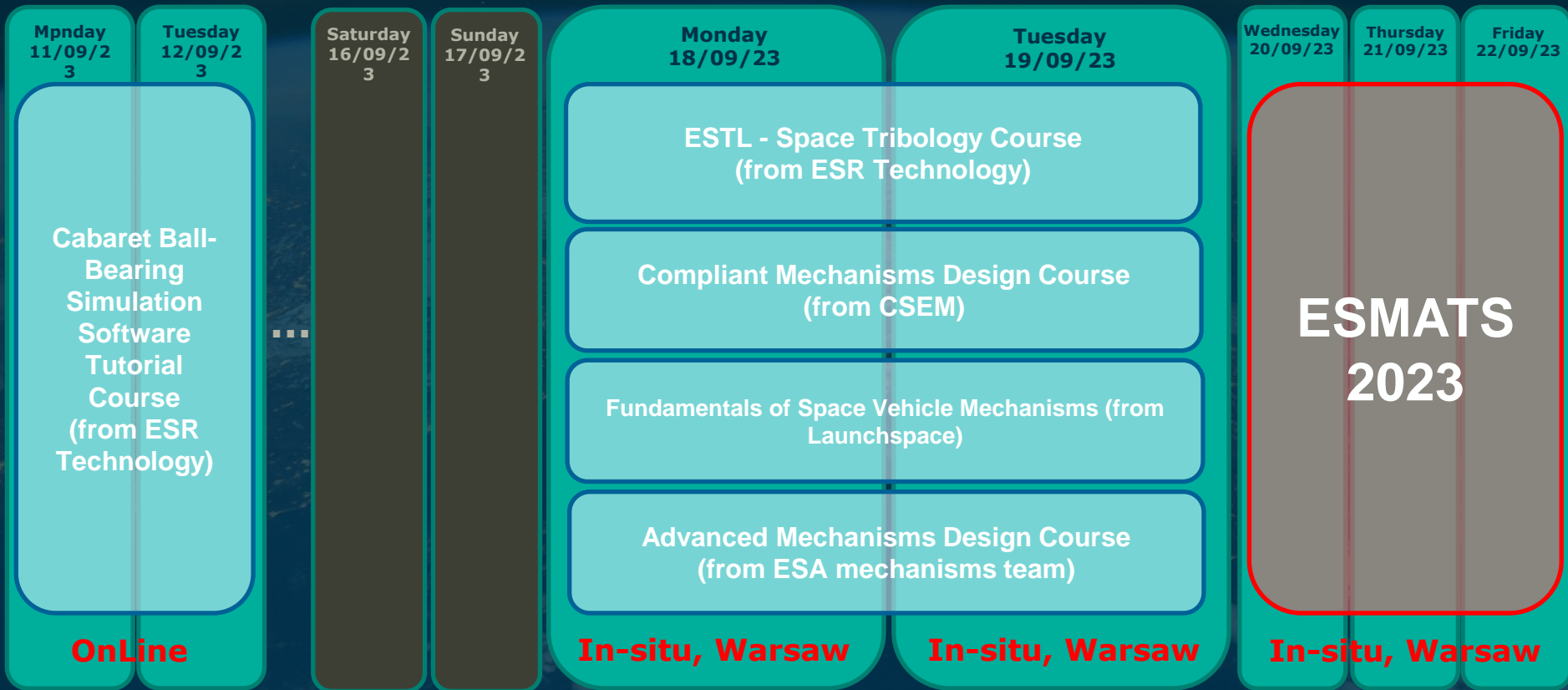
|| csem

esmats
2025

24th – 26th September 2025
Lausanne Switzerland



20th ESMATS 2023 related courses schedule



Advanced Mechanisms Design course (from the ESA team)



- **AGENDA in 2021**
- Gear technology for Space Application
- Long term storage of Space mechanisms, Considerations for Tribological Components and Magnets
- Ball Bearing Technology - Part 1: "Draw me a bearing and justify its performances"
- Model philosophy and test including Logic development
- Electrical Motors for space applications
- Bushings
- Hardware Post-Test Inspection; Pass/Fail Criteria
- Position Sensors for Space mechanisms
- Life Testing of Spacecraft Mechanisms
- Design for Demise (D4D) for Space Mechanisms
- A Mechanisms Perspective on Microvibration
- Motorisation Margins
- Space Mechanisms System Engineering
- Reliability/statistics on mechanisms
- Vibration Tests of Mechanisms
- Pyrotechnics Shock Assessment for Mechanisms
- Errors Analysis for Accurate Positioning
- Advanced Dynamics Simulations for Space Mechanisms
- Ball Bearing Technology - Part 2: Advanced Considerations
- Appendages design and verification
- Piezo actuators
- Hold-down and release mechanisms, Design, Analysis and Test considerations
- Closed Loop Control



Prevention of potential problems!

Following on from the successful AMDC at previous ESMATS in 2017, 2019 and 2021 (on-line), ESA Mechanisms Section is proud to announce their updated training course on 'Advanced Mechanisms Design'. This course will give some practical information for understanding, in greater detail, the main specificities of these technologies, in order to help the designers to be aware of the potential pitfalls when designing Space mechanisms. Rather than giving some closed solutions to a particular problem, this course will provide proper technical understanding of several important mechanisms fields, such that preventive actions can be put in place before a problem occur, and would need expansive and time demanding action to solve the encountered problem in a curative way.

| 2023 | Start Time | End Time | | AMDC Training course topics | Presenters | Time |
|-------|------------|----------|---|--|-----------------------|--------|
| Day 1 | 9:00 | 9:15 | | Course package delivery and in-situ registration | | 15 min |
| | 9:15 | 9:30 | 0 | Welcome and Introduction | Lionel | 15 min |
| | 9:30 | 10:10 | 1 | Space Mechanisms System Engineering (and how to win a contract) | Manfred | 40 min |
| | 10:10 | 10:10 | 2 | New ECSS presentation | only slides (Florian) | 0 min |
| | 10:10 | 10:35 | 3 | Model philosophy and test including Logic development | Ewelina | 25 min |
| | 10:35 | 10:50 | | PAUSE | | 15 min |
| | 10:50 | 11:55 | 4 | Ball Bearing Technology - Part 1: Bearings Technology for Space Application Overview of space bearing solutions for guiding function in rotation, with contact. Specific insight in ball bearings. | Alain | 65 min |
| | 11:55 | 12:30 | 5 | Ball Bearing Technology - Part 2: Advanced Considerations | René | 35 min |
| | 12:30 | 13:15 | 6 | Position Sensors for Space mechanisms | Fernando | 45 min |
| | 13:15 | 14:15 | | Lunch break | | 60 min |
| | 14:15 | 15:20 | 7 | Gear technology for Space Applications | Adam | 65 min |
| | 15:20 | 16:20 | 8 | Electrical Motors for space applications (Part1) | Claudia | 60 min |
| | 16:20 | 16:35 | | PAUSE | | 15 min |
| | 16:35 | 17:35 | 9 | Electrical Motors for space applications (Part2) | Cristina | 60 min |
| 17:35 | 17:55 | 10 | Piezo actuators | Ronan | 20 min | |
| 17:55 | 18:15 | 11 | Smart Material Overview | Kobyé | 20 min | |
| Day 2 | 9:00 | 10:05 | 12 | Motorisation Margins | Joe | 65 min |
| | 10:05 | 10:55 | 13 | Errors Analysis for Accurate Positioning | Paolo | 50 min |
| | 10:55 | 11:10 | | PAUSE | | 15 min |
| | 11:10 | 11:30 | 14 | Vibration Tests of Mechanisms | Ewelina | 20 min |
| | 11:30 | 11:50 | 15 | Pyrotechnics Shock Assessment for Mechanisms | Massimo | 20 min |
| | 11:50 | 12:35 | 16 | Hold-down and release mechanisms, Design, Analysis and Test considerations | Sandro | 45 min |
| | 12:35 | 13:00 | 17 | Appendages design and verification | Ronan | 25 min |
| | 13:00 | 14:00 | | Lunch break | | 60 min |
| | 14:00 | 14:30 | 18 | Life Testing of Spacecraft Mechanisms | Asier | 30 min |
| | 14:30 | 15:00 | 19 | Hardware Post-Test Inspection; Pass/Fail Criteria | Asier | 30 min |
| | 15:00 | 15:00 | 20 | Advanced Dynamics Simulations for Space Mechanisms | Only Slides (Philipp) | 0 min |
| | 15:00 | 16:10 | 21 | A Mechanisms Perspective on Microvibration | Geert & Sandro | 70 min |
| | 16:10 | 16:25 | | PAUSE | | 15 min |
| | 16:25 | 16:50 | 22 | Reliability/statistics on mechanisms | Massimo | 25 min |
| 16:50 | 17:05 | 23 | Long term storage of Space mechanisms, Considerations for Tribological Components and Magnets | Adam | 15 min | |
| 17:05 | 17:25 | 24 | Design for Demise (D4D) for Space Mechanisms | Geert | 20 min | |
| 17:25 | 17:55 | 25 | Closed Loop Control | Stefan | 30 min | |
| 17:55 | 18:15 | | SURVEY completion, Certificate delivery, Control loop Demo | All participants | 20 min | |



Space Tribology Course (STC) - from ESTL



The course will cover the following subjects:

Fundamentals of Tribology – in which tribological concepts are introduced and the special considerations for space and vacuum tribology highlighted.

Tribo-component Design and Performance – in which an overview of the different types, characteristics and performances of tribo-components (ball bearings, gears, plain and ball/rollerscrews, etc.) used in spacecraft applications is provided. This includes a detailed presentation of considerations for design, selection and load capacity verification of ball bearings for space applications.

Materials for Tribo-Contacts – in which an overview of the main categories of materials and their use in spacecraft tribo-components and surfaces is presented.

Lubrication of Spacecraft Components – in which the application-driven considerations for selection of fluid or dry (solid) lubricants for tribo-components and surfaces are provided.

This part includes the considerations and typical performances of dry (solid) and fluid lubricants, respectively. Some practical issues concerning application, handling and preloading of ball bearings and testing of mechanisms where tribological performance is critical are also presented.

Lessons Learned – presenting a selection of the (sometimes painful!) lessons learned on various programmes. The course is presented by experienced staff from ESTL with over 50+ combined years

of space tribological experience and will be valuable both for younger engineers entering the industry and for the more experienced who may wish to refresh or challenge their tribological understanding.

Compliant Mechanisms Design Course – from CSEM



The course will cover the following subjects:

- Introduction to compliant mechanisms
- Presentation of space applications using compliant mechanisms
- Design principles
- Finite Element Modeling guidelines
- Material and lifetime aspects
- Manufacturing guidelines, including recent additive manufacturing advances
- Failure modes and preventions
- Integration and testing guidelines
- Sensor and actuator selection and integration
- Control aspects

Compliant Mechanisms (CM) are proposed to achieve macroscopic linear and rotary motion without friction, wear, backlash, and with extremely high fatigue performance thanks to the elastic deformation of flexible structures. They are used in harsh environments such as vacuum, cryogenic and space where friction is to be avoided while high-precision and a high lifetime are required.

While the potential of CM in space has already been proven over many years, their development can still be challenging. This course will address the complete development aspects for compliant mechanisms, comprising of design and analysis, manufacturing, assembly and testing. The recent advances on CM brought by additive manufacturing will also be presented.

This course is intended for engineers involved in the design, manufacturing and testing, for managers and anyone else interested in having a practical knowledge of the advantages and challenges of compliant mechanisms. This course will give some practical information for understanding, in greater detail, the main specificities of these technologies,

Fundamentals of Space Vehicle Mechanisms – From LaunchSpace



This course is at the right level for someone:

- With less than 15 years of experience with space mechanisms
- Who is responsible for the design of aerospace mechanisms
- Tasked with analysis activities in thermal or structural elements of mechanisms
- With responsibility for developing drive electronics for mechanisms or
- Tasked with systems work related to implementing mechanisms

Course topics include:

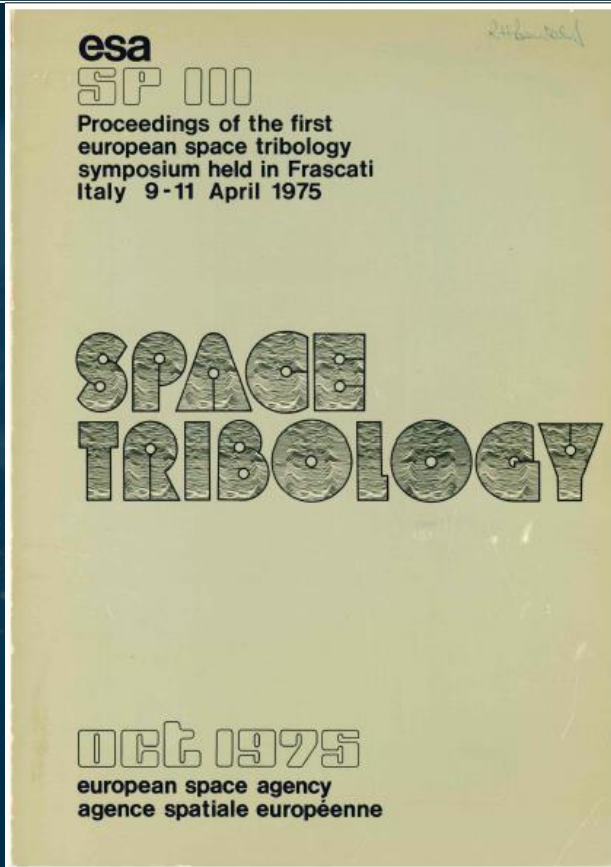
- Mechanisms used in space vehicle
- Pointing subsystems, motors and feedback devices
- Bearings, gears and lubrication fundamentals
- Release and deployment systems
- Power transfer and slip rings
- Mechanisms analysis
- Critical materials for mechanisms
- Spacecraft – mechanism interfaces and sources of mechanism requirements

Fundamentals of Space Vehicle Mechanisms is a special edition of the internationally popular course on this topic.

The instructor, Bill Purdy, explores the technologies required for successful space mechanisms design and offers a detailed look at many of the key components common to most mechanisms. The materials necessary to achieve high performance are discussed. Examples of the many types of mechanisms are included for illustration. In addition, mechanisms' relationships and interfaces with other vehicle systems are explored. The course includes design and analysis examples to demonstrate principles involved in understanding how mechanisms should work and how design margins should be evaluated during the evolution of a programme.

If you want to pick the right type of motor for your application, lubrication for your application or angular measurement device for your application, then this is the right course. You will learn the fundamentals of space mechanisms from a leading mechanisms expert. A unique benefit is the instructor's sharing of his experience and lessons learned.

External Laboratory



European Space Tribology Laboratory (ESTL)

Was established in 1972 ... and still rocking !

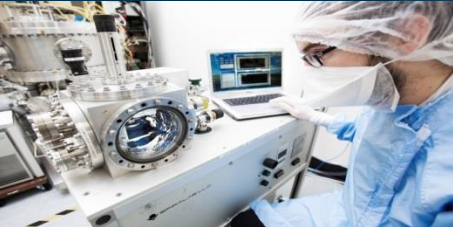
Fundamental objective :

"to increase the efficiency and reliability of spacecraft through the application of good tribology"

-> Minor consultancy

-> Major consultancy

European Space Tribology Laboratory (ESTL) in UK





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aerospace & advanced composites

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Cold Welding
Cold Welding Database
Electro Tribology
Forming Tribometer
Mechanical Testing
Microstructural Characterisation
Composite Materials
Functional Surfaces
Development of Test Methods and Test Equipment
Projects
Partners @ Networks
About us

COLD WELDING DATABASE

Based on the result of "General Validation Studies" a data base was initiated:

- Comparable due to test parameters related to material properties
- It covers the contact modes "impact" and "fretting"
- A summary table shows available material combinations
- For each tests a detailed data sheet is available
- The summary table shows a "classification" related to the severity of adhesion

CONTACT
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+43 2622 90550-300

<http://coldweld.aac-research.at/>

| | | | | | | | | | | | | | | |
|-------------------------|--|-------------------------------|----------------------------------|--------------------------------|---------------------------------|---|---|--|------------------------------|---|-------------------------------------|-------------------------------------|---------------------------|-----------------------------|
| AG/MS2 NO COATING | AL AA219 KEROITE 2ND GEN NO COATING | AL AA7075 NO COATING | AL AA7075 HARD ANODIZED | BRONZE LBS NO COATING | INCONEL 718 NO COATING | STEEL S8 15-5 PH NO COATING | STEEL S8 17-4 PH NO COATING | STEEL S817-7 PH NO COATING | STEEL S817-7 PH TIC | STEEL AISI 52100 NO COATING | STEEL AISI 316L NO COATING | STEEL AISI 440C NO COATING | TI 6AL4V NO COATING | TI IMI 318 NO COATING |
|-------------------------|--|-------------------------------|----------------------------------|--------------------------------|---------------------------------|---|---|--|------------------------------|---|-------------------------------------|-------------------------------------|---------------------------|-----------------------------|

Ag10Cu
no coating

AI
AA2219
Keronite 2-
42U (AR)

AI
AA2219
Keronite 2-
42U (TC)

AI
AA2219
Keronite 3-
17U (AR/TC)

AI
AA2219
Keronite 3-
25U+HCS2
(AR/TC)

AI
AA2219
Keronite 3-
25U (AR/TC)

AI
AA2219
Keronite 3-
25U+HCS2
(AT/TC)

AI
AA6082
Keronite 3-
25U (AR/TC)

AI
AA7075
no coating

AI
AA7075
HCS
plate

AI
AA7075
PH2
AFC0088C

AI
AA7075

Cold Welding

Design criteria acc. ECSS-E-38 Part 04

Results

Design criteria acc. ECSS-E-38 Part 04

• The summary tables are based on following classification:

| Symbol | Adhesion force [mN] | | Comment to adhesion |
|--------|---------------------|-------------|--|
| | lower limit | upper limit | |
| ● | 0 | 200 | No or negligible adhesion, noise of test |
| ◐ | 201 | 500 | Small measurable adhesion |
| ◑ | 501 | 5000 | Strong adhesion |
| ◒ | 5001 | higher | Severe adhesion |